## STUDY OF SEISMIC BEHAVIOUR OF VERTICAL ASYMMETRIC MULTI-STORIED BUILDING

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## ABSTRACT

Seismic Behaviour of asymmetric building may cause interruption of force flow and stress concentration. Due to this, there is produce of torsion in the building which leads to increase in shear force, lateral deflection and ultimately causes failure. Asymmetry can be reason for a buildings poor performance under sever seismic loading. The building with vertical setbacks and L, H, U or T shaped in plans which built as unit are more affected during seismic event. There is horizontal torsional effect on each arm arising from the differential lateral displacement of two ends of each arm. In this paper, inelastic seismic behaviour of multistoried building with vertical setbacks are analyzed by IS code approach .The effect of torsion on building are analyzed. Designs of asymmetric multistoried building are studied. Study shows that there is increase in shear force due to torsion in column and increase in area of steel reinforcement in column particularly at the edge member of the building.

Keywords: Center Of Mass, Center Of Stiffness, Seismic Analysis, Shear Force, Torsion etc.

## I. INTRODUCTION

## 1.1 General

To perform well in an earthquake, a building should possess four main attributes, mainly having simple and regular configuration, adequate lateral strength, stiffness and ductility. Buildings having simple regular geometry and uniformity distributed mass and stiffness in plan as well as in elevation, suffer much less damage than the irregular configuration. A building shall be considered as irregular as per IS 1893-2002, if it lacks symmetry and has discontinuity in geometry, mass or load resisting elements. These irregularities may cause problem in continuty of force flow and stress concentrations. Asymmetrical arrangement of mass and stiffness of elements have increase in shear forces on lateral force resisting elements resulting from the horizontal torsional moment arising due to eccentricity between centers of rigidity.

The study of dynamic torsional effects in buildings, particularly in multi-storey structures where this effect is more pronounced has been possible only with the recent development of programme for the dynamic analysis of three dimensional frame structures. Torsion occurs when the centre of mass does not coincide with the centre of rigidity in a story level. This can be a result of a lack of symmetry in the building plan or random disposition of live loads in an

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otherwise symmetrical structure. Torsion can also be included in symmetrical structures by the rotational components of ground motions.

Structural symmetry can be a major reason for buildings poor performance under severe seismic loading, asymmetry contributes significantly to the potential for translational-torsional coupling in the structures dynamic behaviour which can lead to increased lateral deflections, increased member forces and ultimately the buildings collapse.

Yielding in corner column or end shear wall in buildings due to torsional stresses tends to destroy the symmetry in an originally symmetrical building or increase the eccentricity in an unsymmetrical building, as the centre of resistance moves away from the yielding member. The increase in the eccentricity causes yielding to develop further. This tendency towards magnification of torsional effects by yielding in corner or at end elements suggests that such elements should be designed more conservatively than other member where torsional vibrations can be significant.

Horizontal twisting occurs in buildings when centre of mass and centre of rigidity do not coincide. The distance between these two is called eccentricity (e). Lateral force multiplied by this 'e' cause a' torsional moment which must be resisted by the structure in addition to the normal seismic force. Therefore, the Code stipulates that provision shall be made for increase in shear forces acting on particular elements resulting from the horizontal torsion due to an eccentricity between the centre of mass and the centre of rigidity. It is desirable to plan structural elements of the building in such a way that there is no eccentricity or the building is symmetrically planned with respect to the mass centre. However, it is very difficult to do so in practice and some provision has to be made for it.

Since there could be quite a bit of stiffness's of the variation in computed value of e, it is recommended by the Code that design eccentricity shall be 1.5 e. The net effect of this torsion is to increase shear in certain structural elements and reduction in certain others. The Code recommends that reduction in shear on account of torsion should not be applied and only increased shears in the elements be considered.

#### **Types of Irregularities:**

These irregularities are categorized as follows:

- 1. Vertical Irregularity
  - a. Stiffness Irregularities Soft Storey:
  - b. Mass Irregularities:
  - c. Vertical Geometric Irregularity
- 2. Horizontal/Plan Irregularity
- 3. Torsion Irregularities:
- 4. Re-entrant Corners:
- 5. Diaphragm. Discontinuity:

#### 1.2 General terms

#### 1.2.1 Centre of Mass (C.M)

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According to IS: 1893-2002, centre of mass is the point through which resultant of the masses of a system acts. This point corresponds to centre of gravity of masses of system.

Earthquake induced lateral force on the floor is proportional to mass. Hence, resultant of this force passes through the centre of mass of the floor. Entre of the mass can be located by using method of statics. For floor having uniform distribution of mass, the C.M coincides with geometric centre of building. [7]

$$X = \frac{\sum Mi.Yi}{\sum Mi.}$$

Where,

X, Y= Location of centre of mass

Mi = Lumped mass at i<sup>th</sup> floor

## 1.2.2 Centre of Stiffness or centre of rigidity (C.S):

According to IS1893-2002, centre of stiffness, for a one story building can be defined as the point on the floor through which lateral force should pass in order that floor undergoes only rigid body translation, with no rigid body rotation. In case of multi-story buildings, the concept of centre of stiffness is more complex. In general, for multi-story building C.S at each floor can be defined as-

- a. A lateral load applied at that floor and passing through that point does not cause rotation of that floor (even though it may cause rotation of other floor).
- b. Centre of stiffness of different floors of a building is obtained as these points at which the vertical seismic load profile should be applied such that none of floor undergoes any rotation. According to this definition of C.S, the location of C.S may depend on the vertical load profile for the building.

According to SP-22, the location of centre of stiffness is computed as follows- [7]



Where,

Xr and Yr = Location of centre of stiffness

X and Y = Distance of column line from centre of stiffness

Kx and Ky = Stiffness of the various elements in two directions respectively.

## II. MODELING

Data-

- Slab Thickness = 125 mm
- Size of Beam = 230 mm x 600 mm
- Size of Column = 350 mm x 350 mm
- Height of floor = 3m
- Live load on floors  $= 3 \text{ kN/m}^2$
- Floor Finish  $= 1.0 \text{ kN/m}^2$

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- Grade of Concrete  $= 20 \text{ N/mm}^2$
- Grade of Steel  $= 415 \text{ N/mm}^2$
- EI = Constant
- Seismic zone = III
- Zone Factor (Z) = 0.16
- Importance Factor (I) = 1.0
- Response Reduction Factor (R) = 5.0
- Type of Soil = Medium
- Damping = 5%

#### **2.1 Design of Members**

Following loads have been considered for the design of the structure

Dead Load (DL)

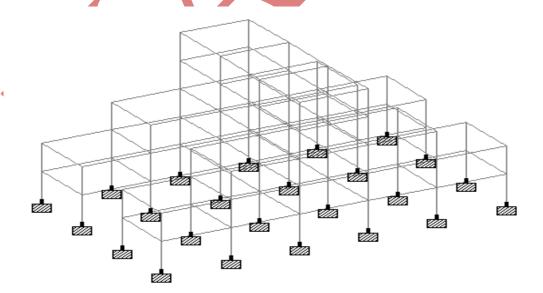
Live Load (LL)

Earthquake Load (EQ)

• Load combinations:

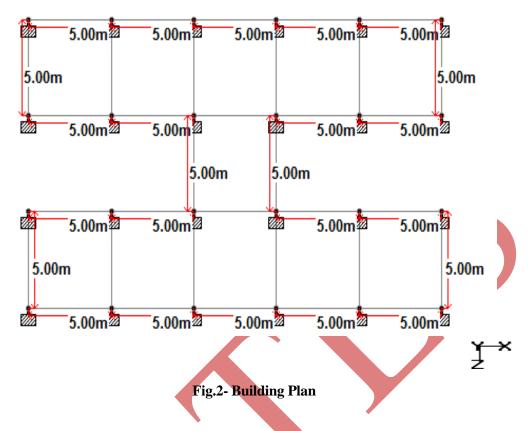
According to IS 1893:2002, following load combinations have been considered,

- I. 1.5 DL + 1.5 LL
- II. DL + 1.2 LL + 1.2 EQ
- III. DL + 1.2 LL 1.2 EQ



**Fig.1- Building Frame with Irregular Profile** 

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#### III. RESULTS AND DISCUSSION

#### 3.1 Comparative Results of Displacement -

	Table.1Comparative R	Results of Dis	placement without and	With Considering Torsion.
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NODE NO.	MAXIMUM DISPLACEMENT WITHOUT CONSIDERING TORSION (MM)	MAXIMUM DISPLACEMENT WITH CONSIDERING TORSION (MM)
101	12.185	12.430
102	12.185	12.393
103	9.337	10.010
104	9.299	9.972

Comparative Results of maximum displacements in the building are studied in number Table.1, which shows that there is increase in the displacement due to torsion than that of without torsion and similarly Comparative Results of Shear force in column when earthquake force in X and Z direction are studied in Table.2, which shows that there is increase in the Shear force due to torsion than that of without torsion.

## 3.2 Comparative Results shear force in column

Table.2 Comparative result of Shear in column without considering Torsion and Shear in column
with considering Torsion (X and Z direction)

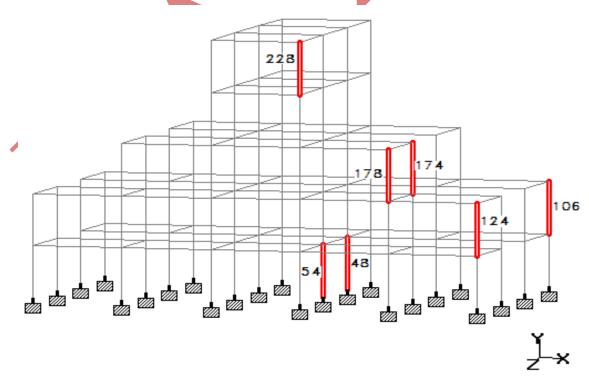
NODE NO.	EARTHQUAKE FOR	CE IN X DIRECTION	EARTHQUAKE FORCE IN Z DIRECTION			
	SHEAR IN COLUMN WITHOUT TORSION(KN)	SHEAR IN COLUMN WITH TORSION (KN)	SHEAR IN COLUMN WITHOUT TORSION(KN)	SHEAR IN COLUMN WITH TORSION (KN)		
1	18.472	18.958	9.338	8.253		
2	8.61	7.554	28.087	24.96		
3	15.007	13.375	53.862	53.222		
4	21.514	19.088	45.028	46.23		
5	5.714	4.956	26.785	30.238		
6	13.981	14.343	13.33	13.961		
7	22.045	22.337	9.647	8.705		
8	10.678	10.145	27.659	24.698		
9	23.435	22.755	7.375	7.043		
10	30.477	29.438	8.891	9.443		
11	7.209	6.811	26.135	29.632		
12	16.252	16.487	12.952	13.78		
13	22.045	21.756	9.647	8.705		
14	10.678	11.214	27.659	24.698		
15	23.435	24.169	7.375	7.043		
16	30.477	31.542	8.891	9.443		
17	7.209	7.614	26.135	29.632		
18	16.252	16.019	12.952	13.78		
19	18,472	17.995	9.338	8.253		
20	8.61	9.678	28.087	24.96		
21	15.007	17.052	53.862	53.222		
22	21.514	24.119	45.028	46.23		
23	5.714	6.494	26.785	30.238		
24	13.981	13.625	13.33	13.961		

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## 3.3 Comparative study of Column design when earthquake force in X-direction

COLU MN	DESIGN OF COLUMN WITHOUT TORSION			DESIGN OF COLUMN WITH TORSION			VARIATION IN % OF
NO.	$A_{st} (mm^2)$	Main Rein.	Lateral Ties	A <sub>st</sub> (mm <sup>2</sup> )	Main Rein.	Lateral Ties	STEEL
48	1372	4-20 dia.	8mm dia. @300mm c/c	1405	12-12 dia.	8mm dia. @300mm c/c	2.41
54	1372	8-16 dia.	8mm dia. @190mm c/c	1448.50	12-16 dia.	8mm dia. @190mm c/c	5.58
106	1431.23	8-16 dia.	8mm dia. @255mm c/c	1490.73	8-16dia.	8mm dia. @255mm c/c	4.16
124	1488.76	8-16 dia.	8mm dia. @190mm c/c	1478.73	12-16 dia.	8mm dia. @190mm c/c	0.69
174	1561.71	8-16dia.	8mm dia. @255mm c/c	1583.81	8-16 dia.	8mm dia. @255mm c/c	1.41
178	1318.86	4-25 dia.	8mm dia. @300mm c/c	1380.47	20-12 dia.	8mm dia. @190mm c/c	4.67
228	1636.06	16- 12dia.	8mm dia. @190mm c/c	1720.98	16-12dia.	8mm dia. @190mm c/c	5.19

## Table.3 Comparative Results of Column Design when Earthquake force in X–Direction.



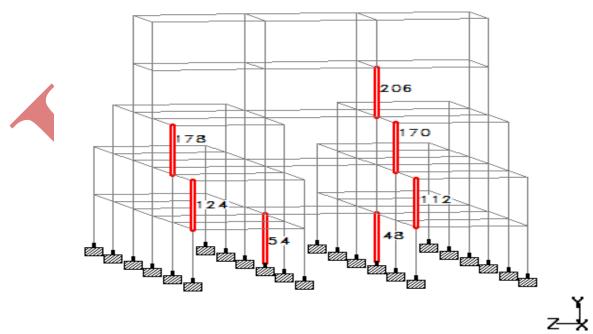


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## 3.4 Comparative study of Column design when earthquake force in Z-direction

DESIGN OF COLUMN WITHOUT TORSION			DESIGN OF COLUMN WITH TORSION			VARIATION IN % OF
A <sub>st</sub> (mm <sup>2</sup> )	Main Rein.	Lateral Ties	A <sub>st</sub> (mm <sup>2</sup> )	Main Rein.	Lateral Ties	STEEL
1470	8-16 dia.	8mm dia. @255mm c/c	1568	8-16 dia.	8mm dia. @255mm c/c	6.67
1470	8-16 dia.	8mm dia. @255mm c/c	1568	8-16 dia.	8mm dia. @255mm c/c	6.67
1371.26	8-16 dia.	8mm dia. @255mm c/c	1400	8-16dia.	8mm dia. @255mm c/c	2.09
1380.90	4-20 dia.	8mm dia. @300mm c/c	1498.32	8-16 dia.	8mm dia. @255mm c/c	8.50
1234.69	4-20 dia.	8mm dia. @255mm c/c	1303.52	12-12 dia.	8mm dia. @190mm c/c	5.57
1088.30	4-20 dia.	8mm dia. @300mm c/c	1172.38	4-20 dia.	8mm dia. @300mm c/c	7.73
1560.28	8-16- dia.	8mm dia. @255mm c/c	1670.99	8-16 dia.	8mm dia. @255mm c/c	7.09
	A <sub>st</sub> (mm <sup>2</sup> ) 1470 1470 1371.26 1380.90 1234.69 1088.30	Ast (mm²) Main Rein.   1470 8-16 dia.   1470 8-16 dia.   1470 8-16 dia.   1371.26 8-16 dia.   1380.90 4-20 dia.   1234.69 4-20 dia.   1088.30 4-20 dia.   1560.28 8-16-	A <sub>st</sub> (mm <sup>2</sup> )   Main Rein.   Lateral Ties     1470   8-16 dia.   8mm dia. @255mm c/c     1470   8-16 dia.   8mm dia. @255mm c/c     1470   8-16 dia.   8mm dia. @255mm c/c     1371.26   8-16 dia.   8mm dia. @255mm c/c     1380.90   4-20 dia.   8mm dia. @300mm c/c     1234.69   4-20 dia.   8mm dia. @300mm c/c     1088.30   4-20 dia.   8mm dia. @300mm c/c     1560 28   8-16-   8mm dia.	Ast (mm <sup>2</sup> )   Main Rein.   Lateral Ties   Ast (mm <sup>2</sup> )     1470   8-16 dia.   8mm dia. @255mm c/c   1568     1470   8-16 dia.   8mm dia. @255mm c/c   1568     1470   8-16 dia.   8mm dia. @255mm c/c   1568     1371.26   8-16 dia.   8mm dia. @255mm c/c   1400     1380.90   4-20 dia.   8mm dia. @300mm c/c   1498.32     1234.69   4-20 dia.   8mm dia. @255mm c/c   1303.52     1088.30   4-20 dia.   8mm dia. @300mm c/c   1172.38     1560 28   8-16-   8mm dia.   1670.99	TORSIONTORSION $A_{st}$ (mm²)Main Rein.Lateral Ties $A_{st}$ (mm²)Main Rein.1470 $8-16$ dia. $8mm$ dia. ( $@255mm$ c/c)1568 $8-16$ dia.1470 $8-16$ dia. $8mm$ dia. ( $@255mm$ c/c)1568 $8-16$ dia.1470 $8-16$ dia. $8mm$ dia. ( $@255mm$ c/c)1568 $8-16$ dia.1371.26 $8-16$ dia. $8mm$ dia. ( $@255mm$ c/c)1400 $8-16dia$ .1380.90 $4-20$ dia. $8mm$ dia. ( $@300mm$ c/c)1498.32 $8-16$ dia.1234.69 $4-20$ dia. $8mm$ dia. ( $@255mm$ c/c)1303.52 $12-12$ dia.1088.30 $4-20$ dia. $8mm$ dia. ( $@300mm$ c/c) $1172.38$ $4-20$ dia.1560.28 $8-16 8mm$ dia. $8mm$ dia. $1670.99$ $8-16$	TORSION   TORSION   TORSION     Ast (mm <sup>2</sup> )   Main Rein.   Lateral Ties   Ast (mm <sup>2</sup> )   Main Rein.   Lateral Ties     1470   8-16 dia.   8mm dia. @255mm c/c   1568   8-16 dia.   8mm dia. @255mm c/c     1470   8-16 dia.   8mm dia. @255mm c/c   1568   8-16 dia.   8mm dia. @255mm c/c     1470   8-16 dia.   8mm dia. @255mm c/c   1568   8-16 dia.   8mm dia. @255mm c/c     1371.26   8-16 dia.   8mm dia. @255mm c/c   1400   8-16dia.   8mm dia. @255mm c/c     1380.90   4-20 dia.   8mm dia. @300mm c/c   1498.32   8-16 dia.   8mm dia. @255mm c/c     1234.69   4-20 dia.   8mm dia. @255mm c/c   1303.52   12-12 dia.   8mm dia. @190mm c/c     1088.30   4-20 dia.   8mm dia. @300mm c/c   1172.38   4-20 dia.   8mm dia. @300mm c/c     1560 28   8-16-   8mm dia.   1670.99   8-16   8mm dia.

### Table.3 Comparative Results of Column Design when Earthquake force in Z–Direction.





www.ijates.com ISSN (online): 2348 – 7550

#### **IV. ACKNOWLEDGEMENTS**

I would like to extend my deepest gratitude to my supervisor **Dr. P. S. Patil** for giving me the opportunity to do an M-Tech. at the Rajarambapu Institute of Technology, Rajaramnagar. I am greatly indebted to him for his continuing confidence in me as well as for giving me constant support throughout these years. It was a great experience to work with him and his valuable suggestions made me to have deep interest and knowledge of the topic. I have learnt many things from his rich academic and practical experience.

#### V. CONCLUSION

The following Conclusions were made from this study.

- 1. Study shows that there is increase in shear force due to torsion produces in column by irregularity.
- 2. There is 4.53 % increase in the displacement due to torsion.
- 3. There is increase in steel reinforcement in some of the columns particularly at the corners due to asymmetry of building.
- 4. There is increase in reinforcement due to torsion when earthquake force in Z direction than Earthquake force in X direction.

#### REFERENCES

- Dutta S. C. and Roy R. "Seismic Demand of Low-Rise Multistory Systems with general Journal of Engineering Mechanics, 138 (7) 2012, 311-318.
- [2] Goel R. K.) "Seismic Response of Asymmetric systems: Energy-Based Approach." Journal of Structural Engineering, 123 (11) 1997, 1444-1453.
- [3] Soo Y. and Stafford B. S. "Assessment of Translational-Torsional coupling in Asymmetric Uniform Wallframe Structures." Journal of Structural Engineering, 121 (10) 1995, 1488-1496.
- [4] Tabatabaei R. and Saffari H. "Evaluation of the Torsional Response of Multi story Buildings using Equivalent Static Eccentricity", Journal of Structural Engineering, vol-137, 2011, 862-868.
- [5] Wai K. Tso (1990). "Static Eccentricity Concept for Torsional Moment Estimations", Journal of Structural Engineering, 117 (3) 1990, 1199-1212.

#### Codes

- [6] Criteria for Earthquake Resistant Design of Structures-IS 1893 (Part 1):2000.
- [7] Explanatory handbook on codes for Earthquake Engineering, SP-22.

#### Books

- [8] Earthquake Resistance Design of Structures,-Dr.S.K.Duggal.
- [9] Dynamics of structure theory and applications to Earthquake Engineering- Anil K. Chopra.