

# INFLUENCE OF DIFFERENT PARAMETERS TOWARDS MILLING BURR MINIMIZATION AT WET CONDITION

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## ABSTRACT

Undesirable burrs are created in most of the machining processes. A burr is a plastically deformed material that remains attached at the workpiece edges after machining, and must be removed for making the parts to function effectively. The main objective of the present work is to explore the suitable condition to obtain minimum or negligible burr around the edge of a machined product at wet condition. In this work, experiments have been carried out on a vertical axis CNC milling machine to perform face milling on aluminium alloy (Alloy-4600M) blocks with single inserted coated carbide tool on a 54 mm diameter cutter for observing the nature of burr formation.

**Keyword:** Aluminium alloy, Burr, Carbide Tool, CNC Milling Machine, Wet condition

## I. INTRODUCTION

A burr is a plastically deformed material that remains attached at the workpiece edges after machining. It is often in the form of a rough strip of metal present at the edge of the workpiece adjacent to the machined surface. Burrs must be removed for making the parts to function effectively [1]. Material removal by milling process is considered as one of the most multipurpose and extensively used machining processes. Burrs generated in workpiece produced by milling operation is a serious concern because the presence of burr on the cutting edges could significantly affect the cutting performance. A clear understanding of burr formation mechanism would be of great importance in minimizing burr, and hence, would improve manufacture of precision jobs. Silva et al. [2] investigated the burr formation mechanisms at the edges (lateral and exit) during face milling of mould steel using carbide tools. They proposed that burrs were minimised by optimizing the cutting conditions like cutting speed (Vc), feed per tooth (fz) and depth of cut (doc).

Chern [1] experimentally found the different types of burr formed, which is highly dependent on the in-plane exit angle,  $\psi$ . Five types of burrs were created and observed in the experiments, they are knife-type burr, wave-type burr, curl-type burr, edge breakout burr, and secondary burr. Shefelbine and Dornfeld [3] stated that in case of dry machining, burr formation was larger because of increased ductility at elevated temperatures. But, Heisel et al. [4] experimentally found with the reference material C45E as well as some comparative materials that the influence of minimum quantity lubrication on burr formation in face milling. The burr value increased in machining with minimum quantity lubrication compared to dry machining.

A study carried out [5] in the German automotive and machine tool industries showed costs associated with burr minimization, deburring and part cleaning. To evaluate the economic impact of expenses caused by burrs, participants of the survey were asked to name the manufacturing share related to burrs for a specific workpiece.

Expenses were caused by an increase of about 15% in man power and cycle times. In addition, 2% share in the reject rate and 4% share in machine breakdown times due to burrs, were reported. Control and removal of burrs are one of the important issues in many machining operations and have been in the focus of research in cutting operations for the last 50 years.

The main objective of the present work is to explore suitable machining condition to obtain minimum or negligible burr formation on a machined product at wet condition, using water soluble Blasocut Combi as cutting fluid. Observation on influence of different cutting velocities ( $V_c$ ), feeds ( $S_o$ ), and in-plane exit angles ( $\psi$ ) on the burr formation in face milling of aluminium alloy with  $0^\circ$  and  $15^\circ$  exit edge bevel angel, keeping depth of cut ( $t$ ) constant for all machining conditions and observed the burr formation mechanism.

## II. EXPERIMENTAL PROCEDURE

Experiments have been carried out on a vertical axis CNC milling machine to perform face milling on aluminium alloy (Alloy-4600M) blocks with single inserted coated carbide tool on a 54 mm diameter cutter for observing nature of burr formation. Depth of cut ( $t$ ) has been maintained constant at 3 mm for all sets of experiments. All sets of experiments have been performed in wet condition. In each experiment set, at first, in-plane exit angles are varied from  $30^\circ$  to  $90^\circ$  at a step of  $30^\circ$  with respect to three different feeds ( $S_o$ ) 0.08 mm/tooth, 0.1 mm/tooth and 0.12 mm/tooth respectively. Then, this set of experiments have been repeated at three different cutting velocity ( $V_c$ ) of 339 m/min, 237 m/min and 170 m/min respectively without any exit edge bevel angle to find out the condition for minimum burr formation. Next, these all sets of experiments which are done without any exit edge bevel angle have been performed with  $15^\circ$  exit edge bevel angle. Beveling of exit edge is made using the shaping machine (make – Pathak Industries, Howrah). As Saha et al. [6] found that an optimum value of exit edge bevel angle is  $15^\circ$ , and Das et al. [7] observed negligible burr at in-plane exit angle of  $60^\circ$  for a workpiece having exit edge bevel angle of  $15^\circ$  at dry condition. The bevel is made of a height of 3 mm. After machining in wet condition, exit edges of workpieces are observed under a Mitutoyo, Japan make tool makers microscope (Model No.: T510), and the height of burr is measured



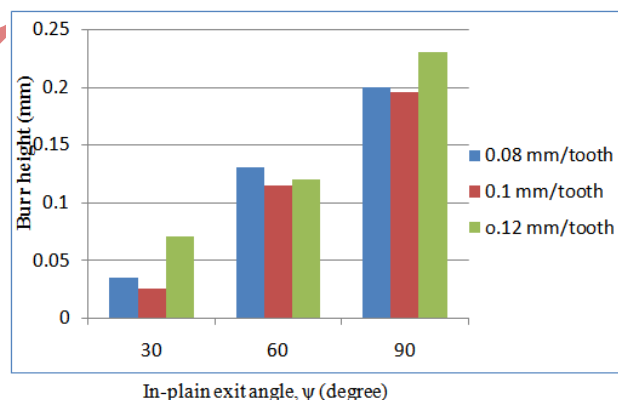
**Figure 2.1: Photographic view of vertical axis CNC milling machine**

**Table 2.1: Experimental Details**

Machine Tools	Vertical Axis CNC Milling Machine. Make: Bharat Fritz Werner, India. Type: Akshara VF30CNC, Sl. No.: 5081/269.
Cutting Tool	TiN Coated Carbide Insert for Face Milling (Single Insert). Cutter Diameter: 54mm. Make: Sandvik Asia Ltd., India. Cutter Specification: 490-054Q22-08M241259 Insert Specification: 490R-08T308M-PM
Job Material	Aluminum Alloy (Alloy 4600M) Hardness: 30 HRA. Composition: Cu (0.1%), Si (12.0%), Mg (0.1%), Mn (0.5%), Ni (0.1%), Zn (0.1%), Pb (0.1%), Sn (0.1%), Ti (0.1%), Fe (0.1%) and Al (remaining). Size: 79mm × 72mm × 46mm.
In-plain exit angle (°)	30, 60, 90
Exit edge bevel angle (°)	0 & 15
Cutting velocity ( $V_c$ ) (m/min)	339
Feed ( $S_o$ ) (mm/tooth)	0.08, 0.1, 0.12
Depth of cut (t) (mm)	3
Environment	Wet (Cutting Oil: Blasocut Combi, Make: Blaser Swisslube, Swetzerland.)

## 2.1 Experimental Investigation for Set 1 without Edge Bevel

Face milling operation has been performed on aluminium alloy (Alloy-4600M) test pieces with a milling cutter of diameter 54 mm, where depth of cut (t) and cutting velocity ( $V_c$ ) are constant at 3mm and 339 m/min respectively, but feed ( $S_o$ ) is varied thrice. In this set of experiment, in-plain exit angle is varied from 30° to 90° at a step of 30° without exit edge bevel. Microscopic views of burrs are shown in Fig.2.3 (a-i). It is found that burr height at the exit edge is quite less at 30° in-plane exit angle, under 339 m/min cutting velocity under all the three feeds of 0.08 mm/tooth, 0.1 mm/tooth and 0.12 mm/tooth without any edge bevel. Among all the three, feeds 0.1 mm/tooth gives lest burr height.



**Figure 2.2: Variation of average height of burrs for set 1**

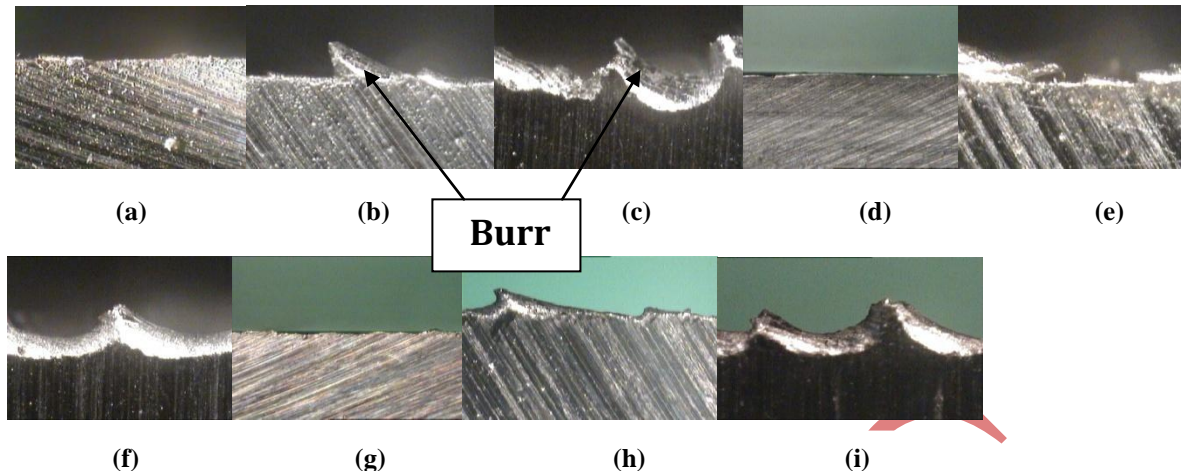


Figure 2.3: Microscopic views of burrs (in 20X) for in-plane exit angle and feed of (a)  $30^\circ$  and 0.08 mm/tooth, (b)  $60^\circ$  and 0.08 mm/tooth, (c)  $90^\circ$  and 0.08 mm/tooth, (d)  $30^\circ$  and 0.1 mm/tooth, (e)  $60^\circ$  and 0.1 mm/tooth, (f)  $90^\circ$  and 0.1 mm/tooth, (g)  $30^\circ$  and 0.12 mm/tooth, (h)  $60^\circ$  and 0.12 mm/tooth, (i)  $90^\circ$  and 0.12 mm/tooth respectively of experiment set 1.

## 2.2 Experimental Investigation for Set 2 with Edge Bevel Angle $15^\circ$

In experimental set 2 the cutting velocity ( $V_c$ ) of 339 m/min, feed ( $S_o$ ) and in-plane exit angle are varied three times with provision of  $15^\circ$  exit edge bevel angle. Burr heights measured are presented in Fig.2.4. Microscopic views of burrs are shown in Fig.2.5 (a-i).

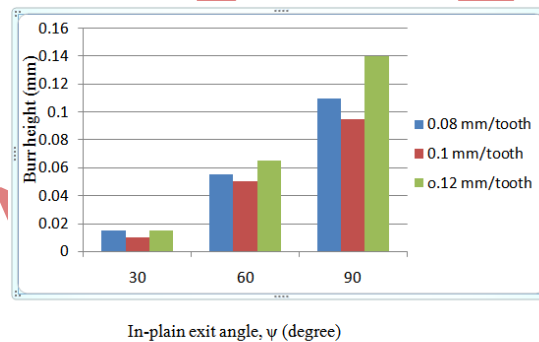


Figure 2.4: Variation of average height of burrs for set 2

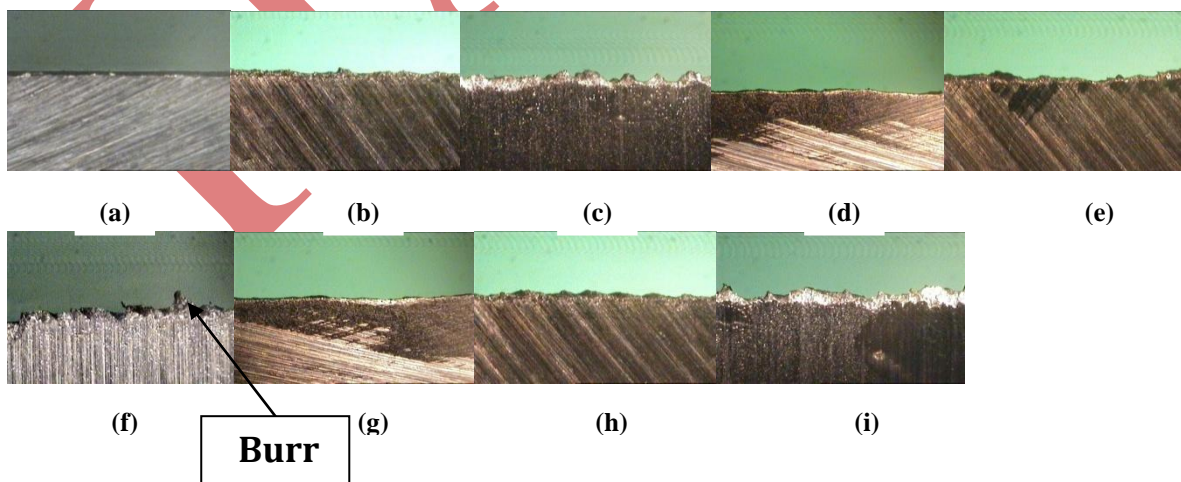


Figure 2.5: Microscopic views of burrs (in 20X) for in-plane exit angle and feed of (a)  $30^\circ$  and 0.08 mm/tooth, (b)  $60^\circ$  and 0.08 mm/tooth, (c)  $90^\circ$  and 0.08 mm/tooth, (d)  $30^\circ$  and 0.1 mm/tooth, (e)  $60^\circ$  and 0.1 mm/tooth, (f)  $90^\circ$  and 0.1 mm/tooth, (g)  $30^\circ$  and 0.12 mm/tooth, (h)  $60^\circ$  and 0.12 mm/tooth, (i)  $90^\circ$  and 0.12 mm/tooth respectively of experiment set 2.

### III. CONCLUSION

On the basis of the experimental investigation in face milling carried out in this work, following conclusions may be drawn.

1. Among the three in-plane exit angle ( $\psi$ ) undertaken, in-plane exit angle of  $30^\circ$  gives quite less burr formation with the exit edge bevel angle, of  $0^\circ$  and  $15^\circ$  at wet environment using TiN coated carbide tool under all speed-feed condition.
2. At the medium feed ( $S_o$ ) condition of 0.1 mm/tooth and high cutting velocity ( $V_c$ ) of 339 m/min, observed burr height at an in-plane exit angle of  $30^\circ$  for a workpiece having exit edge bevel angle of  $15^\circ$  is the lowest in this experimental work, and may be considered negligible. At a low in-plane exit angle, the need of backup support material is less, and therefore, the chance of burr formation becomes negligible. Low exit edge bevel also reduces requirement of backup support, due to gradual decrease in depth of cut. So, for this reason, burr formation is negligible at low in-plane exit angle, and at somewhat low exit edge bevel angle.

### REFERENCES

- [1] G.L. Chern, 2006, 'Experimental Observation and Analysis of Burr Formation Mechanisms in Face Milling of Aluminium Alloys', International Journal of Machine Tools & Manufacture, Vol. 46, pp. 1517–1525.
- [2] J.D. Silva, F.P. Saramango, A.R. Machado, 2009, 'Optimization of the Cutting Conditions for Burr Minimization in Face Milling of Mould Steel', Journal of the Braz. Soc. Of Mech. Sci. and Eng., Vol. XXXI, No. 2, pp. 151-160.
- [3] W. Shefelbine, D Dornfeld, 2004, 'The Effect of Dry Machining on Burr Size', Laboratory for Manufacturing and Sustainability, pp. 1-5.
- [4] S. Heisel, M. Schaal, G. Wolf, 2009, 'Burr Formation in Milling with Minimum Quantity Lubrication', German Academic Society for Production Engineering, Vol. 3, No. 1, pp. 23-30.
- [5] J.C. Aurich, D. Dornfeld, P.J. Arrazola, V. Franke, L. Leitz, S. Min, 2009, 'Burrs—Analysis, Control and Removal', CIRP Annals - Manufacturing Technology, Vol.58, pp. 519–542.
- [6] S.P Pratim and S. Das, 2011, 'Burr Minimization in Face Milling: an Edge Beveling Approach', J. Engineering Manufacturing, Vol. 225, Part B, pp. 1528-1534.
- [7] P.P. Saha, D. Das, and S. Das, 2007, 'Effect of Edge Beveling on Burr Formation in Face Milling', Proceedings of the 35th MATADOR conference, Taiwan, pp. 199-202.